



MARKED-UP VERSION OF

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A METHOD AND APPARATUS FOR CONTROLLING ~~THE~~ HEAD VELOCITY INOF A DISK ~~HARD~~-DRIVE DURING RAMP LOAD/UNLOAD

5

FIELD OF THE INVENTION

The present invention relates to ~~a method and apparatus for controlling the transducer head velocity in~~of a disk drive during a ramp load or unload procedure.

- 10 ~~More particularly, the present invention provides for the control of the transducer heads using a microprocessor to determine the speed of the heads and, accordingly, to make velocity adjustments.~~

BACKGROUND OF THE INVENTION

- 15 ~~A hard disk drives include is a device with one or more disks, or platters,~~ on which digital information is stored ~~as in the form of~~ magnetic charges. The disk (or disks) is are mounted on and rotated by a cylindrical spindle rotated by a spindle motor assembly. An actuator assembly includes an actuator arm and Contemporary hard disk drives typically include an actuator, a rotary actuator structure that is powered by a voice coil motor ("VCM"). The, an actuator arm
- 20 extending from the VCM and supports a slider that includes a read/write head. The head reads from and writes to the disk as the slider flies over the disk on an air cushion. T, he VCM positions the head and a transducer head disposed at the end of the actuator arm. The rotary actuator structure positions one or more slider head assemblies at desired locations relative to the surfaces of the
- 25 ~~magnetic disk or disks. A hard disk read/write head, which is used to read and~~

write the data to and from the magnetic disk, is mounted onto the slider head assembly. Thus, the slider physically supports the head and holds it in the correct position relative to the hard disk platter as the head floats over the surface. While the actuator assembly is actuated by a VCM, a spindle motor
5 rotates the magnetic disk or disks.

~~In modern disk drives have been designed the heads with a landing zone are generally parked, or stopped, at the inner diameter of the disk to park the head. The , such as a landing zone, whenever the spindle assembly is at rest. A landing zone is an area of the disk that is designated as either a takeoff or~~
10 ~~landing spot for the heads as while the disk spindle starts spinning or stops spinning, moving respectively. As Once the disk spindle starts spinning motor begins to accelerate, the read/write heads is are dragged onto the disks until the disks accelerate to a reaches a speed that creates sufficient air pressure for at which the heads to will fly, or separate, from and fly over the disk platter.~~

~~To minimize the friction between the read/write head and the hard disk, the surface of the disk can have is usually textured to create a "rough" texture surface to minimize friction between the head and the disk in the landing zone. However, as disk drive . As the storage capacity of hard disk drives increases every year, the flying height of the read/write heads decreases, and the disk is~~
20 ~~given a . Thus, a hard disk surface must be very smooth texture to avoid damaging either the heads and/or the disk drive. The smooth texture dramatically increases If, for example, the heads are parked onto the smooth surface of the disk, the contact friction between the head and the disk in the landing zone increases dramatically. As a result, an increased spindle motor in~~
25 ~~current may be required to break the head loose from the disk drive to allow the disk spindle to rotate, or spin up.~~

~~This concern is relevant today as manufacturers of modern disk drives have are increasingly designing smaller form factors, or disk sizes, (2.5", 1.8" and 1" so far). Small form factors are useful , particularly in battery-operated~~
30 ~~devices where i. An increased spindle motor in the current to spin up the disk is~~

required to rotate the spindle is therefore unnot desirable. SAdditionally, a smaller form factors reduces the disk surface area and the total disk data area, which is reduced further by if a separate landing zone is employed. SFinally, smaller form factors disk drives are also more susceptible to operational and non-
 5 operational shock, which could be more damaging if the head and the disk are in contact. Thus, small form factors are penalized by a landing zone.

DTo overcome these constraints, disk drives have been designed with manufacturers have implemented a ramp to avoid a landing zone. The structure where the heads are lifted off the disk and are parked onto a separate ramp. In a
 10 ramp structure, the read/write heads do not fall to the surface of the disk when the disk's motor stops. Rather, the heads is are lifted off from the surface of the disk while the drive is still spinning and unloaded are parked on the to special ramp while the disk is spinning, and then s. After the read/write heads have ascended the ramp, the disks decelerates and stops spinning. When the power is
 15 reapplied to the spindle motor, the process is reversed. The disks spins up, and once the disks have sufficient accelerated to a speed for such that the head to fly without contacting the disk surface, the heads is loaded from are moved off the ramps and positioned over onto the surface of the disk platters.

During a ramp load/unload procedure, the head velocity of the read/write
 20 head is accurately controlled to avoid damaging the head, or the disk at athe contact point of contact, thereby compromising the disk drive reliability and quality. As the VCM actuator coil moves through its magnetic poles, it generates a back electromotive field (EMF_{bemf}) voltage, ("V_{bemf}"), which is proportional to its speed. Thus, e back EMF voltage also V_{bemf} is an indicates or of the actuator
 25 velocity and therefore may be accurately measured to provide feedback of the head velocity. The back EMF V_{bemf} voltage (V_{bemf}) can may be calculated based on the total voltage across the VCM (V_{vcm}) and the IR drop across the VCM (I_{vcm} x R_{vcm}) as follows:

$$\underline{V_{bemf} = V_{vcm} - (I_{vcm} \times R_{vcm})} \quad (1)$$

Thus, the back EMF voltage is measured by removing the VCM IR drop from the VCM voltage by first determining the overall voltage across the VCM coil. The total voltage across the VCM coil is: $V_{bemf} + I_{vem} * R_{vem}$. To measure the V_{bemf} , therefore, the term $I_{vem} * R_{vem}$, which represents the VCM "IR" drop, is removed from the equation, thereby isolating the V_{bemf} voltage.

There back EMF voltage can be measured by ~~are two methods by which the V_{bemf} voltage may be isolated and measured.~~ First, a ~~pPulse wWidth mModulation (PWM) technique or may be used.~~ Second, an IR cancellation technique ~~may be employed.~~ In the ~~Pulse Width Modulation ("PWM")~~ technique, the VCM is turned off periodically, forcing the VCM current in the VCM coil, I_{vem} , to go to zero. ~~Since Thus,~~ the "IR" drop across the VCM coil equals zero, and the back EMF V_{bemf} voltage is ~~may be~~ readily measured. In the IR cancellation technique, the back EMF V_{bemf} voltage is determined by measuring the gain ~~of~~ a servo loop. ~~Since Unlike the PWM technique, the current to the VCM current~~ is not periodically turned off ~~in the IR cancellation technique.~~ Rather, some calibrations ~~may be required to cancel the IR drop component from the VCM voltage.~~ ~~The Such~~ calibrations may need to be repeated because temperature and voltage deviations ~~may cause the gain of the servo loop to change frequently over time.~~

Of the two V_{bemf} measurement techniques discussed above, the PWM technique is easier to implement. The PWM technique requires less hardware and fewer calibrations than the IR cancellation technique. However, the load/unload process of the VCM in the PWM technique may generate be audible noise during ramp load/unload and therefore ~~inappropriate for applications in which audible noise is not desirable.~~ The IR cancellation technique, however, ~~may itself not be appropriate for certain applications, as it is more sophisticated than the PWM technique and requires a robust calibration technique with more associated hardware.~~ -Further, an increased voltage in the resolution of the voltage measurements may require a hardware design change to increase

because the resolution and accuracy of the measurements is a function of the number of bits of the analog-to-digital A/D converter.

Disk drives have been ~~In the prior art, hardware had to be specifically~~ designed for either the PWM or IR cancellation techniques. If both techniques were needed for a particular application, two distinct sets of hardware had to be implemented, thereby possibly increasing the overall cost of the system. Further, ~~during the implementation of the measurement techniques, the~~ decision as to which technique would be employed needed to be selected ~~made~~ before prior to any voltage measurements, thereby greatly reducing the system flexibility.

There is, therefore, ~~For the reasons stated above and for other reasons presented in greater detail in the detailed description of the present specification, there is a~~ need for a disk drive with ~~desire for a system that allows for the~~ accurate control of the a disk read/write head during a ramp load/unload procedure. ~~T~~In particular, there is also a need for a disk drive that measures the back EMF voltage with ~~system that may employ either the a PWM technique or the an IR cancellation calibration technique to measure the back emf voltage~~ without the need for hardwiring a specific measurement technique or making multiple system calibrations prior to operation of the disk drive.

SUMMARY OF THE INVENTION

To achieve these and other advantages and in accordance with the ~~purposes of~~ the present invention, as embodied and broadly described, a method and apparatus for controlling the velocity of a ~~read/write disk head~~ during a ramp load/unload are disclosed.

A disk drive controls head velocity during ramp load/unload by measuring voltages across a VCM and a sense resistor in series with the VCM, calculating a

back EMF voltage using the VCM and sense resistor voltages, and adjusting the head velocity using the back EMF voltage.

~~An~~ According to an embodiment of the present invention, a method includes amplifying the VCM and sense resistor voltages, multiplexing the amplified voltages, digitizing the multiplexed voltages and calculating the back EMF voltage in discrete-time based on the digitized voltages.

Another embodiment includes selecting between the PWM and IR cancellation techniques and calculating the back EMF voltage using the selected technique without two distinct sets of hardware.

Another embodiment includes calculating a calibration constant by comparing reference voltages across the VCM and the sense resistor while no current is applied to the VCM with voltages across the VCM and the sense resistor while current is applied to the VCM.

Another embodiment includes calculating a control variable in the discrete time domain using a proportional-integral control technique that compares a target head velocity to an actual head velocity and adjusting the head velocity based on the control variable. ~~for accurately measuring the V_{bemf} voltage using either of two different techniques; PWM and IR cancellation, and a means for making real time adjustments to the velocity of the voice coil motor (VCM) is disclosed. The method includes measuring, amplifying, and transporting to a microprocessor the voltages across a voice coil motor (V_{motor}) and a sense resistor (V_{Rsense}). The method further includes calculating the V_{bemf} voltage of the VCM and making real time adjustments to the VCM velocity.~~

~~According to another embodiment of the present invention, an apparatus to control the velocity of a transducer head during a ramp load/unload is disclosed. The control circuitry includes a driver circuit that powers the VCM, a multiplexer, an analog to digital converter (ADC), and a microprocessor. The microprocessor typically calculates the VCM velocity based on a measured V_{bemf} voltage.~~

BRIEF DESCRIPTION OF THE DRAWINGS

These and other features and advantages of the present invention are more fully described in the following drawings and accompanying text in which like reference numbers represent corresponding elements throughout:

FIG. 1 illustrates a ~~cross-section of a hard-disk drive assembly;~~

FIG. 2 illustrates a ~~block diagram of the art-ramp load/unload procedure;~~

FIG. 3 illustrates a ~~schematic of the-ramp load/unload control circuit in accordance with a preferred embodiment of the present invention;~~

FIG. 4 illustrates a flowchart of a ~~microprocessor-calibration algorithm in accordance with the present invention; and~~

FIG. 5 illustrates a flowchart of a load/unload algorithm ~~in accordance with the invention; and~~

FIG. 6 illustrates a flowchart of a velocity compensation algorithm ~~in accordance with the present invention.~~

DETAILED DESCRIPTION

FIG. 1 illustrates a conventional ~~depicts a prior-art~~ hard-disk drive 100 ~~that~~. The ~~prior-art hard-disk drive 100~~ includes an actuator 110 ~~having a voice coil motor (VCM) 105, a disks 1120, or platters, a cover 11530, an actuator arm 1240, a spindle 1250, a DC power input 130, a read/write heads 13560, a base casting 1470, an I/O connector 145, a printed circuit board 150, a frame/bracket 155, a connector 160, a printed circuit cable 165 and a shock mount 170 and sliders 180.~~

~~The~~ A hard-disk drive 100 uses round flat disks 1120, ~~or platters, that is~~ are coated on both sides with a special-media material ~~that~~ designed to stores information. The disks 1120 ~~is~~ are mounted and stacked onto the cylindrical spindle 1250 that, during operation, rotates the disks 1120 at a high speed. ~~The~~ Electromagnetic read/write heads 13560 ~~is positioned over and are mounted onto the sliders 180 and are used to record or reads information to or from and writes~~

to the disks 1120. The head 135 is embedded in a ~~The sliders 180 are mounted~~
onto the actuator arms 1240. The VCM 105 and the actuator arm 120 form an
actuator assembly that ~~are connected mechanically into a single assembly and~~
~~positioned over the surface of the disk 120. The sliders 180 and the actuator~~
5 ~~arms 140 moves~~ the read/write heads 13560 relative to the disk 110 as needed for
read/write operations. The hard-disk drive 100 is enclosed by the a cover 11530
and ~~a the~~ base casting 1470.

FIG. 2 illustrates ~~A-ramp load/unload in the disk hard-drive 1200 is~~
~~illustrated in FIG. 2. The diskhard drive 1200 includes a ramp 175, and the~~
10 ~~actuator arm 120 includes a lift tab 180. 210, a détente (rest) position 220, an~~
~~actuator 110, an actuator arm 140, a disk 120, a slider 180, a read/write head~~
~~160, and a read/write position 240. During read/write operations, the read/write~~
~~heads 135160 fliesy over the surface of the disk 1120, at a the read/write position~~
~~185240, on as a result of an air cushion caused by the rotation of the disks 1120.~~
15 During the-ramp unload, the VCM 105 actuator 110 moves the slider 180 and
read/write-head 13560 from the disk 110 onto the special-ramp 175210 while the
disk 1120 is still spinning.

~~—The read/write head 160 comes to rest at the détente position 220, which is~~
~~used by the hard disk drive 200 as a landing zone on the hard drive 200. After~~
20 ~~the read/write-head 13560 comes to rest at a onto the park détente-position 19220,~~
~~the hard-disk drive 1200 stops the rotation of the disk 1120. Similarly, during~~
~~the-ramp load, the hard-disk drive 1200 spins up increases the rotation of the~~
~~disk 1120, and w. When the disk 1120 is spinsning at sufficient a-velocity for~~
~~where the read/write-head 13560 to can fly above the disk 1120 without making~~
25 ~~contact, the VCM actuator 10510 moves the slider 180 and read/write-head 13560~~
~~from off the special-ramp 175 210 to and onto the disk 1120.~~

FIG. 3 illustrates ~~In order to control the velocity of the slider and the~~
~~read/write head 160 up and down the ramp 210, one embodiment of the present~~
~~invention uses a ramp load/unload control circuitry 300. The control circuitry~~
30 ~~300 includes a driver circuit 30510, a first operational amplifier 310, a second~~

operational amplifier 315, that powers the VCM, a multiplexer 320, an analog-to-digital converter (ADC) 325, and a microprocessor 330.

The VCM 105 has an internal resistance (R_{vcm}), a back EMF voltage (V_{bemf}) and a total voltage (V_{vcm}). The VCM 105 is connected in series with a sense resistor 195 with a sense resistance (R_{sense}).

The driver 305 has a first output that is connected to the VCM 105 and a positive input of the first operational amplifier 310, and a second output that is connected to the sense resistor 195 and a negative input of the second operational amplifier 315. The VCM 105 is connected to the sense resistor 195, a negative input of the first operational amplifier 310 and a positive input of the second operational amplifier 315 at a node.

The driver 305 powers the VCM 105 by sending a current through the VCM 105 and the sense resistor 195. The first operational amplifier 310 receives and amplifies the total voltage across the VCM 105 (V_{vcm}). The second operational amplifier 315 receives and amplifies the voltage across the sense resistor 195 (V_{rsense}). The multiplexer 320 selects between the amplified VCM voltage from the first operational amplifier 310 at a first voltage path and the amplified sense resistor voltage from the second operational amplifier 315 at a second voltage path in response to a sample signal from the microprocessor 330. The ADC 325 converts the multiplexed voltage selected by the multiplexer 320 from analog to digital format, and sends the digital signal along a serial port to the microprocessor 330.

The microprocessor 330 calculates the back EMF voltage based on the VCM voltage and the sense resistor voltage, as amplified by the operational amplifiers 310 and 315, multiplexed by the multiplexer 320 and digitized by the ADC 325. The microprocessor 330 also typically calculates the VCM velocity based on the back EMF voltage, and sends a control signal to the driver 105 in a feedback loop to accurately control the head velocity.

The microprocessor 330 calculates the back EMF voltage by selecting between a measured V_{bemf} voltage 340. There are two methods by which the back

~~emf voltage may be isolated and measured. First, the PWM technique and the Pulse Width Modulation may be used. Second, the IR cancellation technique may be employed. As a result, the disk drive 100 calculates the back EMF voltage using a selected one of the PWM technique and the IR cancellation technique~~
5 ~~without implementing two distinct sets of hardware.~~

~~In the Pulse Width Modulation ("PWM") technique, the VCM is turned off periodically, forcing the current in the VCM coil, I_{vem} , to go to zero. Thus, the "IR" drop across the VCM coil equals zero and the bemf voltage, V_{bemf} , is readily measured. Unlike the PWM technique, the current to the VCM is not~~

10 ~~periodically turned off in the IR cancellation technique. Rather, some calibrations may be required to cancel the IR component from the VCM voltage. Such calibrations may need to be repeated because temperature and voltage deviations may cause the gain of the servo loop to change frequently over time. After it calculates the V_{bemf} voltage, the microprocessor 390 performs a control~~
15 ~~loop compensation before controlling the input to the driver circuitry 310. The output of a driver circuit 310 is connected to both a resistance of the voice coil motor, R_{vem} , 320 and the positive input of a first operational amplifier 350.~~

~~When the read/write heads 160 are moved across the magnetic disk, the back emf voltage, V_{bemf} 340, opposes the motion of the heads 160. As the velocity of actuator arm 140 increases, the magnitude of V_{bemf} increases. To measure this~~
20 ~~voltage, an external sense resistor, R_{sense} 330 may be placed in series with V_{bemf} 340 and R_{vem} , 320. R_{sense} 330 may then be connected to the negative input of the first operational amplifier 350 and to the positive input of a second operational amplifier 360. The other side of R_{sense} 330 may be connected to the~~
25 ~~negative input of the second operational amplifier 360 and to an output of the driver circuit 310.~~

~~The output of the first operational amplifier 350 and the output of the second operational amplifier 360 are coupled to a multiplexer 370. The operational amplifiers 350 and 360 output signals are referenced to a Reference~~
30 ~~voltage, V_{ref} 357. An analog to digital converter (ADC) 380 converts the~~

~~multiplexed analog signals into a digital format before they are received by microprocessor 390. The microprocessor 390 calculates the VCM velocity, as described below in Figure 4, does the desired control loop compensation, and sends the appropriate control signal to the input of the driver circuit 310.~~

5 ~~When the disk drive is initialized at power up, the driver circuit 310 is off and the current to the VCM, I_{vcm} , is zero. At this point, the transducer heads are stationary, and the back emf voltage, V_{bemf} 340, is 0. The microprocessor 390 receives a voltage level from the first operational amplifier 350, V_{vem} 353, which is equal to V_{ref} 357, and designates the voltage as V_{ref1} . The microprocessor 390~~
 10 ~~then receives a voltage level from the second operational amplifier 360, which is equal to V_{ref} 357, and designates it as V_{ref2} . To determine the exact offset in each path, V_{ref} is measured through the paths of V_{vem} 353 and the sense resistor, V_{Rsense} .~~

~~The microprocessor 390 then determines the output level in both paths of V_{vem} 353 and V_{Rsense} 355 for the ADC 380 voltage corresponding to no current flowing in the VCM coils. The microprocessor 390 calibrates the control circuitry 300 using the calibration algorithm 400 described below. Theis method of calibration algorithm 400 calculates the gain calibration constant
 15 ~~gain coefficient, (K_{cal}), using the following IR cancellation technique:~~~~

20 ~~K_{cal} may be defined as:~~

$$\text{---} K_{cal} = \frac{i \times R_{vcm} \times K_{vcm}}{i \times R_{sense} \times K_{sense}} \text{---} \text{(Equation 21)}$$

21)

~~if $K_{vcm} = 1$ -and $K_{sense} = 1$ then~~

$$\text{---} K_{cal} = \frac{i \times R_{vcm}}{i \times R_{sense}}$$

25 ~~(Equation 32)~~

At start-up, a small VCM current is applied towards the outer crash stop making the back EMF voltage zero V_{bemf} 340 = 0:

$$\text{_____ } i \times R_{vcm} = V_{vcm} - V_{ref1}, \text{ and } \text{_____}$$

(Equation 34)

$$\text{_____ } i \times R_{sense} = V_{sense} - V_{ref2}$$

(Equation 4)

5 Therefore, the following relationship ~~is~~ may be established:

$$\text{_____ } i \times R_{vcm} = Kcal \times (i \times R_{sense})$$

(Equation 5)

Substitution yields the following equality:

$$\text{_____ } -(V_{vcm} - V_{ref1}) = Kcal \times (V_{sense} - V_{ref2})$$

10 (Equation 6)

Thus, the microprocessor 3390 ~~may~~ calibrates the control circuit 300 by determining the calibration constant (~~gain coefficient~~ Kcal) as follows:

$$\text{_____ } Kcal = \frac{V_{vcm} - V_{ref1}}{V_{sense} - V_{ref2}}$$

(Equation 7)

15 After calibrating the control circuit 300, the microprocessor 3390 monitors the back EMF voltage V_{bemf} 340, at sample times, to determine whether to increase or decrease the current controlling the ~~read/write head~~ 160 velocity.

Figure 4 illustrates a flow chart of a calibration algorithm 400 that the control circuit 300 ~~control circuit 300 implement~~ initiates to determine a the gain calibration constant (Kcal) at power-up of the disk drive 100. At step 405, ~~t~~ The calibration algorithm 400 starts at step 410. At step 4120, the driver 305 turns off the current to the VCM 105 coil is turned off. At step 415, ~~t~~ The microprocessor 3390 measures the VCM voltage (V_{vcm}) and the sense resistor voltage (V_{sense}) to provide a first reference voltage (V_{ref1}) and a second reference
20 voltage (V_{ref2}) respectively ~~output of the ADC 380 through both the V_{vcm} 353 and V_{sense} 355 paths to determine the reference voltage corresponding to each path, step 425~~. At step 420, the driver 305 applies a ~~A small current is then applied to the VCM 105 to~~ urgemove the read/write heads 13560 in the unload direction (towards a crash stop, away from the disk 110). At step 425, the

multiplexer 320 selects the VCM voltage (V_{vcm}), and at step 430, the multiplexer 320 selects the sense resistor voltage (V_{rsense}). At step 435, before the microprocessor 390 selects and reads the VCM voltage, V_{vcm} 353, step 440. The microprocessor 390 selects and reads the sense voltage, V_{rsense} 355, step 450. In step 460, the microprocessor 390 calculates the calibration constant, K_{cal} , (Kcal) according to aequation (8):

$$K_{cal} = \frac{V_{vcm} - V_{ref1}}{V_{rsense} - V_{ref2}} \quad \text{(Equation-8)}$$

The calibration algorithm 400 ends at step 470.

Figure 5 illustrates a flow chart of a load/unload algorithm 500 that the control circuitry 300 implements to control the velocity of the read/write heads 13560 during rampa load/unload procedure, as illustrated in Figure-2. At step 505, the load/unload The algorithm starts at step 505. At step 510, the microprocessor 390 determines whether the read/write-heads 13560 is are being loaded from or unloaded ontofrom the ramp 175, step 510. If the heads 135 is are being loaded from the ramp 175, then at step 515 the microprocessor 390 sets the voltage corresponding to thea target velocity of the read/write-heads 13560 (as V_{load_target} Load_Target), step 515. At step 520, the microprocessor 390 measures the VCM voltage (V_{vcm}) and the sense resistor voltage (V_{rsense})then receives the V_{vcm} 353 and V_{rsense} 355 voltages from the ADC 380, step 520. At In step 525, the microprocessor 390 calculates the back EMFemf voltage (V_{bemf} bemf 340), as follows:

$$V_{bemf} = (V_{vcm} - V_{ref1}) - K_{cal} \times (V_{rsense} - V_{ref2}) \quad \text{(Equation-9)}$$

AtIn step 530, the microprocessor 390 uses the calculated value for V_{bemf} 340 to determine a velocity error (V_{err}) as follows:

$$V_{err} = V_{loadtarget} - Load_Target - V_{bemf} \quad \text{(Equation-10)}$$

AtIn step 535, the microprocessor 390 performs thea velocity compensation algorithm 600 as-described below in Figure-6 to make adjustments

to the read/write head velocity of the head 13560. ~~The velocity compensation algorithm adjusts the transducer head velocity by comparing the voltage corresponding to the load target velocity with the voltage corresponding to the actual velocity of the transducer heads, as determined from V_{bemf} 340.~~

5 ~~At~~In step 540, the microprocessor 3390 determines whether the read/write heads 13560 ~~is~~ have loaded on to the disk 1120. If the loading procedure is not complete, ~~then at step 545 the microprocessor 3390 waits for the next sampling period and then the process returns to step 520~~one sample duration in step 547 before ~~transferring control to step 520 to measure~~ receive the next VCM voltage
10 ~~(V_{vc}) and sense resistor voltage (V_{rsense}) V_{vc} 353 and V_{Rsense} 355 voltages from the ADC 380. If the loading procedure of the read/write head onto the disk is complete, then at step 550 the head 135 is locked into tracking mode and at step 595 the heads are locked into tracking mode, in step 545, before the load/unload algorithm 500~~endsecludes at step 590.

15 ~~Returning to~~In step 5150, if the microprocessor 3390 determines that the read/write heads 13560 ~~is~~are being unloaded onto the ramp 175210, then at step 555 the microprocessor 3390 ~~sets the voltage corresponding to~~ assigns the target velocity of the head 135 ($V_{unloadtarget}$)as V_{Unload_Target} . ~~At step 560, the microprocessor 330 measures the VCM voltage (V_{vc}) and the sense resistor voltage (V_{rsense}). The microprocessor 390 then receives the V_{vc} 353 and V_{Rsense} 355 voltages from the ADC 380 in step 555. At step 565~~In step 560, the microprocessor 3390 ~~may~~calculates the back EMF voltage (V_{bemf}) ~~V_{bemf} 340~~ according to equation (9):

$$\text{---} V_{bemf} = (V_{vc} - V_{ref1}) - K_{eal} \times (V_{rsense} - V_{ref2}) \text{---} \text{(Equation 9)}$$

25 ~~At~~ Using the calculated value for V_{bemf} 340, in step 57065 the microprocessor 3390 ~~calculates~~ may determine the velocity error ($-V_{err}$), as follows:

$$\text{---} V_{err} = V_{u_Unload_Target} - V_{bemf} - V_{bemf}$$

(Equation 11)

At step 575, ~~t~~The microprocessor 3390 ~~then~~ performs the velocity compensation algorithm 600 as described below in Figure 6 to ~~make any necessary adjustments to the velocity of the read/write head 13560 velocity, step 570.~~ The velocity compensation algorithm adjusts the velocity of the transducer heads by comparing the voltage corresponding to the load target velocity with the voltage corresponding to the actual velocity of the transducer heads, as determined from V_{bemf} 340.

At step 580, ~~t~~The microprocessor 3390 ~~next~~ determines whether the unloading of the read/write head is unloaded from the disk 110 ~~has successfully completed, step 575.~~ If the unloading procedure ~~is~~ has not completed, ~~then at step 585~~ the microprocessor 3390 waits for ~~the next one sampling period and then the process returns to step 560 to measure the next VCM voltage (V_{vcm}) and sense resistor voltage (V_{rsense}) before transferring control to step 555 to receive the V_{vem} 353 and V_{Rsense} 355 voltage measurements, step 580.~~ -If the unloading procedure ~~is~~ has completed, ~~then at step 590~~ the VCM 105 is disabled ~~and at ,step 5985 t.~~ The load/unload algorithm 500 ends at step 590.

Figure 6 illustrates a flow chart of a ~~the~~ velocity compensation algorithm 600 ~~that initiated by the microprocessor 3390 initiates~~ to correct the velocity of the read/write heads 13560. At step 605, ~~t~~The velocity compensation algorithm 600 begins at step 610. At step 610, ~~t~~The microprocessor 330 ~~first~~ determines the value of the velocity error ($-V_{err}(n)$), for the current sample period, ~~step 620.~~ This may be done, as previously described in steps 530 or 57065 of the load/unload algorithm 500. At step 615

Next, the microprocessor 330 determines ~~the value of~~ a discrete control variable (c , $Control(n)$), that will be used by the driver circuit 3105 to ~~make adjustments to the head velocity.~~ Although ~~there are~~ several methods of velocity compensation ~~that are~~ well known in the art and may be employed in the present invention, the preferred embodiment of ~~the present invention employs a~~ the pProportional-Integral control technique, wherein K_p is a proportional constant and K_i an integral constant. Both K_p and K_i are selected according to the

desired frequency and transient responses for the velocity control loop. The proportional-integral control technique calculates the discrete control variable basic equation, in the continuous time domain, for the velocity compensation algorithm 600 may be represented as follows:

$$5 \quad \text{Output_command} = \left(K_p + \frac{K_i}{S} \right) \times V_{err}$$

(Equation 12)

Although a continuous time domain illustration is shown, the preferred embodiment of the present invention employs a microprocessor 390 that digitally processes the control signals. The above output control equation should therefore
10 be implemented in the discrete time domain. In step 630, therefore, the microprocessor 390 calculates the value for the discrete control variable (Control(n)) in the discrete time domain, using the proportional-integral control technique as follows:

$$\text{Control}(n) = \text{Control}(n-1) + K_i \times (T - K_p) \times V_{err}(n-1) + K_p \times (V_{err}(n));$$

15 (Equation 13)

where (n) denotes the current sample and (n-1) denotes the previous sample. The discrete control variable corrects the head velocity by comparing the voltage corresponding to the target velocity with the voltage corresponding to the actual velocity of the head 135 as determined by the back EMF voltage.

20 — At step 620, the microprocessor 390 then sends the discrete control variable value for Control(n) to the driver circuit 3105, and the driver 305 where adjustments to the head velocity based on the discrete control variable will be initiated, step 640. At step 625, Using the current values for Control(n) and Verr(n), the microprocessor 390 sets the discrete control variable and the
25 velocity error of the current sample (control(n) and Verr(n)) to the previous sample (control(n-1) and Verr(n-1)) for use by the next sample value of Control(n-1) and Verr(n-1) equal to the current values of Control(n) and Verr(n), so that these values may be used for velocity control during the next sample time, step 650. At step 630, the microprocessor 330 determines whether If the velocity

compensation algorithm 600 continues. If so, then the process returns to step 610 for the next sample, otherwise at step 635 control is transferred to step 620 wherein the microprocessor determines the value of the velocity error, $V_{err}(n)$, for the current sample period. The velocity compensation algorithm 600
 5 ~~ends~~ concludes at step 660.

EXAMPLE

The present invention is illustrated by the following. By way of example,
 10 the following calculations represent an illustrative implementation of the present invention. Typical values for the VCM resistance and the sense resistors are as follows may be:

$$\text{R}_{vcm} \text{ 320} = 17.1 \, \Omega$$

$$\text{R}_{sense} \text{ 330} = 1 \, \Omega$$

15 Similarly, the gains of the first operational amplifier 3150 (K_{vcm}), and the second operational amplifier 31560, (K_{rsense}) are as follows may be:

$$\text{K}_{vcm} = 5$$

$$\text{K}_{rsense} = 4$$

The ADC 325 preferred embodiment of the invention utilizes a 12-bits
 20 ADC converter 380 with a full-scale voltage of 5 volts and has the following -
 Thus, the resolution of the preferred ADC converter 380 may be:

$$\text{ADC_resolution} = \frac{\text{ADC_FS_voltage}}{2^{\text{ADC_bits}} - 1} = \frac{5}{2^{12} - 1} = 1.221 \cdot 10^{-3} \text{ V/count}$$

(Equation 14)

The driver 305 provides a reference voltage of 2.5 volts to the sense
 25 resistor 195 and the second operational amplifier 315, V_{ref} 357, when V_{bemf} 340
 $= 0$, may be 2.5 volts when the back EMF voltage is zero. The first and second
 reference voltages Because different offset voltages may exist for the paths of
 V_{vcm} and V_{Rsense} , the reference voltage through each path may not be identical to

~~Vref 357. If (Vref1 and Vref2) are as follows defined as the reference voltages at the ADC 380 for each respective path, these voltages may be:~~

$$\text{_____ } V_{ref1} = 2.520 \text{ volts; and}$$

$$\text{_____ } V_{ref2} = 2.510 \text{ volts.}$$

5 ~~_____ Thus, the ADC 380 counts corresponding to the first and second reference voltages at the first and second voltage for each paths are as follows would be:~~

$$\text{_____ } ADC_V_{ref1_count} = \frac{V_{ref1} \cdot 2^{ADC_bits}}{ADC_FS_voltage} = 2064$$

$$\text{_____ } ADC_V_{ref2_count} = \frac{V_{ref2} \cdot 2^{ADC_bits}}{ADC_FS_voltage} = 2056$$

10 ~~_____ The VCM voltage (Vvcm) when Setting the VCM current (Ivcm)_{vcm} is to 10 mA is as follows may then yield a value for Vvcm 353 of:~~

$$\text{_____ } V_{vcm} = V_{ref1} + I_{vcm} \times R_{vcm} \times$$

$$\text{_____ } K_{vcm} \text{ } V_{vcm} \text{ } 353 = V_{ref1} + I_{vcm} \times R_{vcm} \times K_{vcm}$$

$$\text{_____ } = -2.52 \text{ v} + 10 \text{ mA} \times 17.1 \Omega \times 5$$

$$\text{_____ } = -3.375 \text{ volts}$$

15 ~~_____ The ADC converter 380-count corresponding to this Vvcm voltage 353 is as follows:~~

$$\text{_____ } ADC_V_{vcm_count} = \text{Integer} \left(\frac{V_{vcm} \cdot 2^{ADC_bits}}{ADC_FS_voltage} - ADC_V_{ref1_count} \right)$$

~~(Equation 15)~~

$$\text{_____ } = -(3.375 \text{ v} \times 4096) / 5 \text{ v} - 2064$$

$$20 \text{ _____ } = -701$$

~~_____ The Similarly, the ADC converter 380-count corresponding to the V_{R_{sense}} 355 may be calculated by first determining the value of V_{rsense}_{R_{sense}} 355 is as follows:~~

$$\text{_____ } V_{rsense} = V_{ref2} + I_{vcm} \times R_{sense} \times K_{sense} \text{ _____ (Equation 16)}$$

$$25 \text{ _____ } = 2.51 + 10 \text{ mA} \times 1 \Omega \times 4$$

$$\text{_____ } = -2.55 \text{ volts}$$

This value of V_{Rsense} 355 corresponds to the following ADC 380 count corresponding to V_{rsense} is as follows:

$$ADC_Vrsense_count = Integer \left(\frac{Vrsense.2^{ADC_bits}}{ADC_FS_voltage} - ADC_Vref2_count \right)$$

(Equation 17)

$$= -(2.55 \text{ v} \times 4096) / 5 \text{v} - 2056$$

$$= -33$$

Finally, the value for the calibration constant (gain, K_{cal}), for the preferred embodiment is determined as follows:

$$K_{cal} = \frac{ADC_V_{cm_count}}{ADC_Vrsense_count} \quad \text{(Equation 18)}$$

$$= -700 / 33$$

$$= -21.21$$

It should be understood that the number of bits in the ADC 32580 may be increased if greater accuracy or resolution is desired, or the number of bits in the ADC 380 may be reduced to decrease computational burden.

It will be apparent to those skilled in the art that various modifications and variations can be made to the embodiments described above ~~hard disk drive ramp load/unload methodology~~ without departing from the spirit or the scope of the invention. Thus, it is intended that the present invention covers the modifications and variations of this invention provided that they come within the scope of the any claims and their equivalents.

ABSTRACT

A disk drive controls head velocity during ramp load/unload by measuring voltages across a VCM and a sense resistor in series with the VCM, calculating a back EMF voltage using the VCM and sense resistor voltages, and adjusting the head velocity using the back EMF voltage. An embodiment includes amplifying the VCM and sense resistor voltages, multiplexing the amplified voltages, digitizing the multiplexed voltages and calculating the back EMF voltage in discrete-time based on the digitized voltages. Another embodiment includes selecting between PWM and IR cancellation techniques and calculating the back EMF voltage using the selected technique.

~~The present invention provides a hard drive assembly and a related method for measuring the velocity of a transducer head during a ramp load/unload. To achieve these and other advantages and in accordance with the purposes of the present invention, as embodied and broadly described, a method and apparatus for controlling the velocity of a read/write disk head during a ramp load/unload are disclosed. The method includes measuring, amplifying, and transporting to a microprocessor the voltages across a voice coil motor (V_{motor}) and a sense resistor (V_{Rsense}). The method further includes calculating the V_{bemf} voltage of the VCM and making real time adjustments to the VCM velocity. The apparatus used to control the velocity of a read/write disk head during a ramp load/unload includes a driver circuit that powers the VCM, a multiplexer, an analog to digital converter (ADC), and a microprocessor. The microprocessor typically calculates the VCM velocity based on a measured V_{bemf} voltage.~~